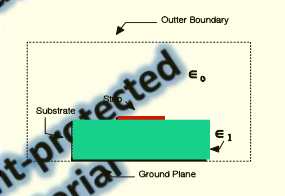


Application of FD to Quasi-Static Solution in Rectangular Coordinates System

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The Application of FD Technique to Quasi-Static Solution of a Microstrip Line Geometry



The boundary conditions for a microstrip line are given by:

- $V = V_1$ on the strip
- $V = 0$ on the ground plane
- $\oint_S \vec{D} \cdot d\vec{s} = 0$ (Gauss's Law) - dielectric interfaces
- Artificial absorbing boundary condition at the outer boundary of the computational domain.



Potential at Nodes on the Interface between Media Without Free Charges

For a 3D problem $\oint_S \vec{D} \cdot d\vec{s} = \rho_{enclosed}$



For a 2D problem

$\oint_l \vec{D} \cdot \hat{n} dl = \rho_{inside}$ where \hat{n} is normal to a closed contour l

Since $\vec{D} = \epsilon \vec{E} = -\epsilon \nabla V = -\epsilon (\frac{\partial V}{\partial x} \hat{x} + \frac{\partial V}{\partial y} \hat{y} + \frac{\partial V}{\partial z} \hat{z})$



On a dielectric interfaces of a 2D problem without free charges,

we get $-\oint_l \epsilon (\frac{\partial V}{\partial x} \hat{x} + \frac{\partial V}{\partial y} \hat{y}) \cdot \hat{n} dl = 0$



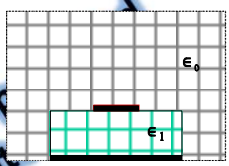
The Application of FD Technique to Quasi-Static Solution of a Microstrip Line Geometry

The solution of the potential will be performed at the nodes of the shown uniform grid inside the computational domain based on the integral form of Gauss's law

$$\oint_V \epsilon \left(\frac{\partial V}{\partial x} \hat{x} + \frac{\partial V}{\partial y} \hat{y} \right) \cdot \hat{n} \, dl = 0$$

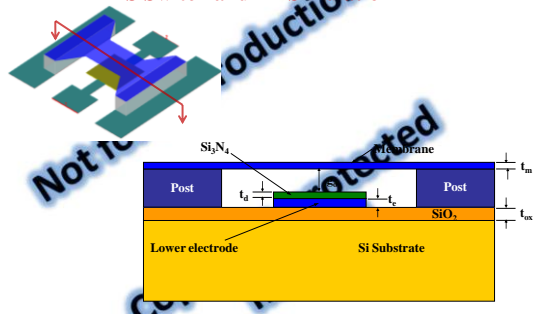
Rather than using Poisson's and/or Laplace's equations

$$\nabla^2 V = -\rho/\epsilon \quad \text{and} \quad \nabla^2 \phi = 0$$



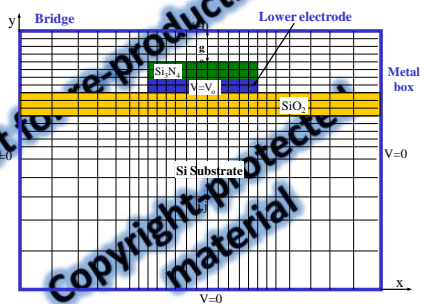
For a more accurate solution, specially for the cases where fine geometrical details are present, it is preferable to use non-uniform grid.

MEMS Switch and 2D Simulation

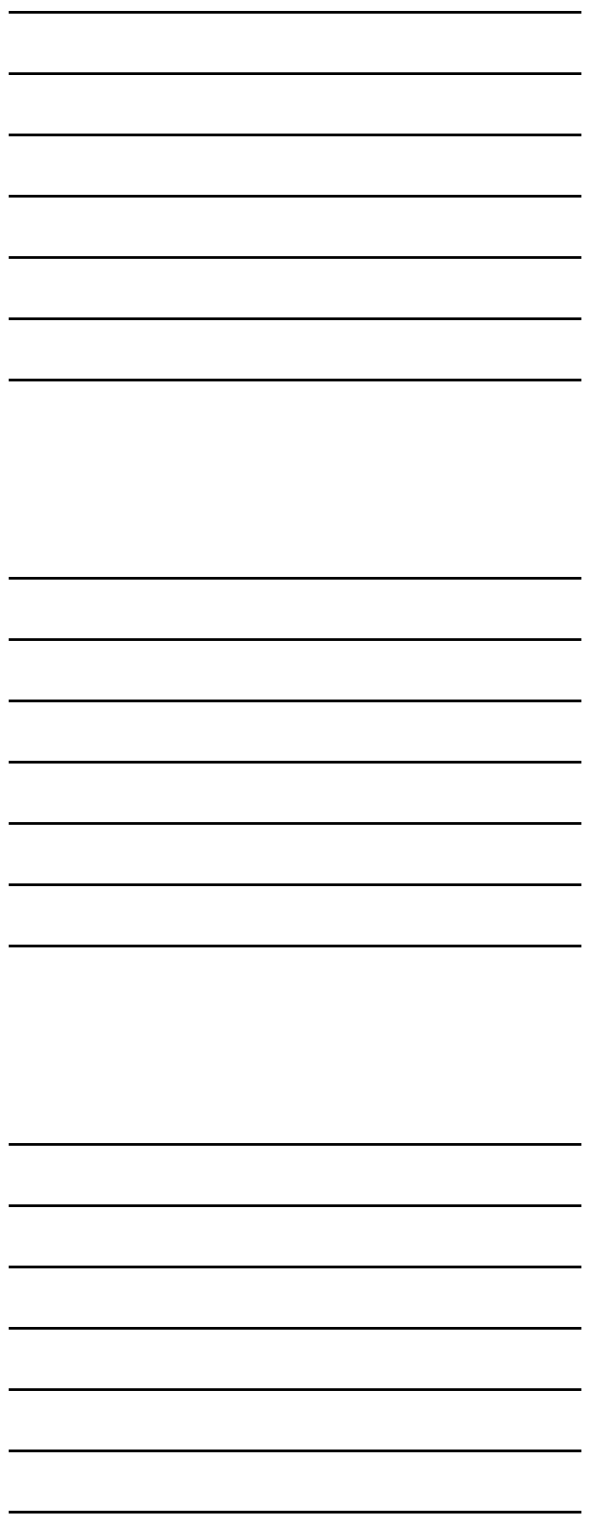


Ehab K. I. Hamad, Atef Z. Elsherbeni, Amr M. E. Safwat, and Abbas S. Omar, "Two-dimensional Coupled Electrostatic-mechanical Model For RF MEMS Switches," ACES Journal, March 2006.

MEMS Switch with Non-Uniform Grid for FD Simulation



Ehab K. I. Hamad, Atef Z. Elsherbeni, Amr M. E. Safwat, and Abbas S. Omar, "Two-dimensional Coupled Electrostatic-mechanical Model For RF MEMS Switches," ACES Journal, March 2006.



Potential at Nodes at The Intersection Between Four Different Media

$$-\oint \epsilon \left(\frac{\partial V}{\partial x} \hat{x} + \frac{\partial V}{\partial y} \hat{y} \right) \cdot \hat{n} dl = 0$$

Non-uniform grid in both x and y directions.

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Potential at Nodes at The Interfaces Between Four Different Media

$$-\oint \epsilon \left(\frac{\partial V}{\partial x} \hat{x} + \frac{\partial V}{\partial y} \hat{y} \right) \cdot \hat{n} dl = 0$$

$$\left[\int_{right} \epsilon(y) \frac{\partial V}{\partial x} dy + \int_{top} \epsilon(x) \frac{\partial V}{\partial y} dx \right] = 0$$

$$\left[- \int_{left} \epsilon(y) \frac{\partial V}{\partial x} dy - \int_{bottom} \epsilon(x) \frac{\partial V}{\partial y} dx \right] = 0$$

Ignore the negative sign on the left side.

$$\frac{V_R - V_C}{x_R - x_C} \left(\frac{\epsilon_1(y_C - y_B)/2 + \epsilon_2(y_C - y_B)/2}{(y_C - y_B)/2} \right) \frac{(y_T - y_C)}{2} + \frac{V_T - V_C}{y_T - y_C} \left(\frac{\epsilon_1(x_C - x_L)/2 + \epsilon_2(x_C - x_L)/2}{(x_C - x_L)/2} \right) \frac{(x_R - x_C)}{2}$$

$$\frac{V_C - V_L}{x_C - x_L} \left(\frac{\epsilon_3(y_C - y_B)/2 + \epsilon_4(y_C - y_B)/2}{(y_C - y_B)/2} \right) \frac{(y_T - y_C)}{2} + \frac{V_C - V_B}{y_C - y_B} \left(\frac{\epsilon_3(x_C - x_L)/2 + \epsilon_4(x_C - x_L)/2}{(x_C - x_L)/2} \right) \frac{(x_R - x_C)}{2} = 0$$

Central Difference

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Potential at Nodes at The Interfaces Between Different Media with Uniform Discretization Along x and y Directions

$$\frac{V_R - V_C}{x_R - x_C} \left(\frac{\epsilon_1(y_C - y_B)/2 + \epsilon_2(y_C - y_B)/2}{(y_C - y_B)/2} \right) + \frac{V_T - V_C}{y_T - y_C} \left(\frac{\epsilon_1(x_C - x_L)/2 + \epsilon_2(x_C - x_L)/2}{(x_C - x_L)/2} \right)$$

$$- \frac{V_C - V_L}{x_C - x_L} \left(\frac{\epsilon_3(y_C - y_B)/2 + \epsilon_4(y_C - y_B)/2}{(y_C - y_B)/2} \right) - \frac{V_C - V_B}{y_C - y_B} \left(\frac{\epsilon_3(x_C - x_L)/2 + \epsilon_4(x_C - x_L)/2}{(x_C - x_L)/2} \right) = 0$$

At a time $\Delta x = \Delta y = h$

$$(V_R - V_C) \left(\frac{\epsilon_1 + \epsilon_2}{2} \right) + (V_T - V_C) \left(\frac{\epsilon_1 + \epsilon_2}{2} \right) - (V_C - V_L) \left(\frac{\epsilon_3 + \epsilon_4}{2} \right) - (V_C - V_B) \left(\frac{\epsilon_3 + \epsilon_4}{2} \right) = 0$$

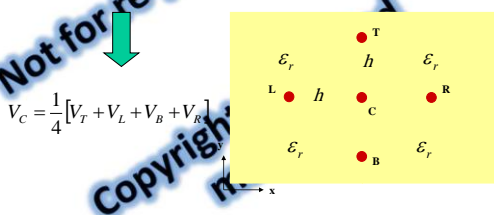
$$V_C = \frac{1}{\epsilon_1 + \epsilon_2 + \epsilon_3 + \epsilon_4} \left[V_T \left(\frac{\epsilon_1 + \epsilon_2}{2} \right) + V_L \left(\frac{\epsilon_1 + \epsilon_2}{2} \right) + V_B \left(\frac{\epsilon_3 + \epsilon_4}{2} \right) + V_R \left(\frac{\epsilon_3 + \epsilon_4}{2} \right) \right]$$

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Potential at Nodes in a Uniform Medium With Uniform Discretization Along x and y Directions

$$V_C = \frac{1}{[\epsilon_1 + \epsilon_2 + \epsilon_3 + \epsilon_4]} \left[V_T \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_L \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_B \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_R \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) \right]$$



$$V_C = \frac{1}{4} [V_T + V_L + V_B + V_R]$$

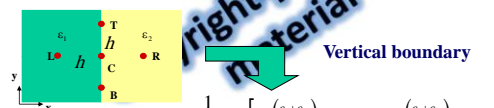
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Potential at The Interfaces Between Two Media With Uniform Discretization Along x and y Directions

General form
$$V_C = \frac{1}{[\epsilon_1 + \epsilon_2 + \epsilon_3 + \epsilon_4]} \left[V_T \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_B \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_R \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) \right]$$



$$V_C = \frac{1}{2[\epsilon_1 + \epsilon_3]} \left[V_T \epsilon_1 \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_B \epsilon_3 + V_R \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) \right]$$

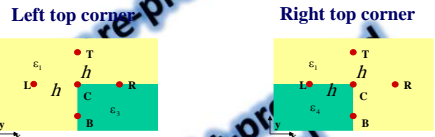


$$V_C = \frac{1}{2[\epsilon_1 + \epsilon_2]} \left[V_T \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_L \epsilon_1 + V_B \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_R \epsilon_2 \right]$$

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Potential at Top Corners With Uniform Discretization Along x and y Directions

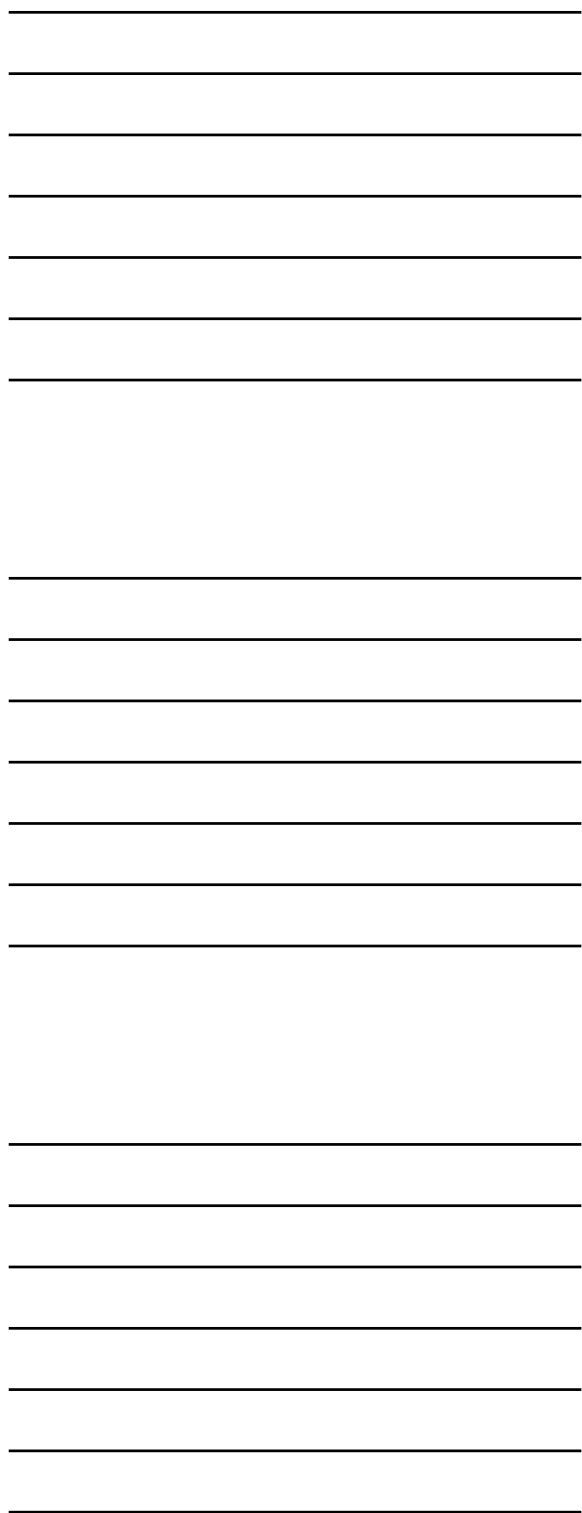
General form
$$V_C = \frac{1}{[\epsilon_1 + \epsilon_2 + \epsilon_3 + \epsilon_4]} \left[V_T \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_B \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_R \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) \right]$$



$$V_C = \frac{1}{[3\epsilon_1 + \epsilon_4]} \left[V_T \epsilon_1 + V_L \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_R \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) \right]$$

$$V_C = \frac{1}{[3\epsilon_1 + \epsilon_4]} \left[V_T \epsilon_1 + V_L \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_B \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_R \epsilon_1 \right]$$

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Potential at Bottom Corners With Uniform Discretization Along x and y Directions

General form
$$V_C = \frac{1}{[\epsilon_1 + \epsilon_2 + \epsilon_3 + \epsilon_4]} \left[V_L \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_B \left(\frac{\epsilon_1 + \epsilon_3}{2} \right) + V_T \left(\frac{\epsilon_2 + \epsilon_4}{2} \right) + V_R \left(\frac{\epsilon_2 + \epsilon_3}{2} \right) \right]$$

$$V_C = \frac{1}{[3\epsilon_1 + \epsilon_2]} \left[V_L \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_B \epsilon_1 + V_R \left(\frac{\epsilon_1 + \epsilon_3}{2} \right) \right]$$

$$V_C = \frac{1}{[\epsilon_1 + 3\epsilon_2]} \left[V_T \left(\frac{\epsilon_2 + \epsilon_4}{2} \right) + V_B \left(\frac{\epsilon_2 + \epsilon_3}{2} \right) + V_R \epsilon_2 \right]$$



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Potential at point on Lines of Symmetry

Symmetry w.r.t. horizontal line

$$\frac{\partial V}{\partial y} = 0 = \frac{V_T - V_B}{2h} \rightarrow V_T = V_B$$

$$V_C = \frac{1}{4} [2V_B + V_L + V_R] \quad V_C = \frac{1}{4} [2V_T + V_L + V_R]$$

Symmetry w.r.t. vertical line

$$\frac{\partial V}{\partial x} = 0 = \frac{V_R - V_L}{2h} \rightarrow V_R = V_L$$

$$V_C = \frac{1}{4} [V_T + 2V_L + V_B] \quad V_C = \frac{1}{4} [V_T + 2V_R + V_B]$$

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Potential at point on Lines of Anti-Symmetry

Symmetry w.r.t. horizontal line

$$V_T = -V_B$$

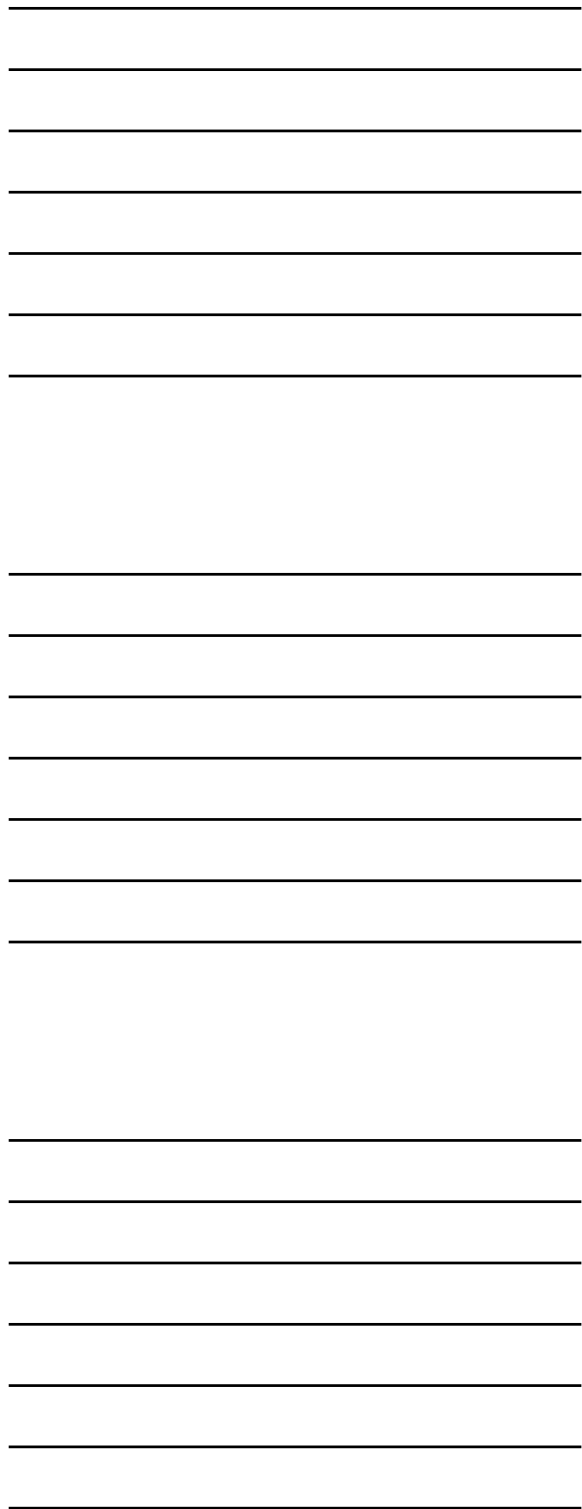
$$V_C = \frac{1}{4} [V_L + V_R] \quad V_C = \frac{1}{4} [V_L + V_R]$$

Symmetry w.r.t. vertical line

$$V_T = -V_L$$

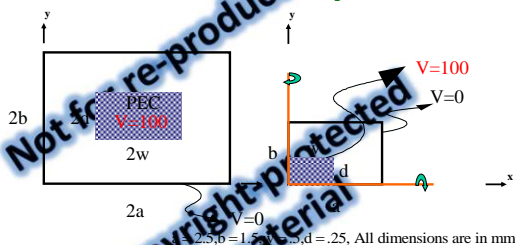
$$V_C = \frac{1}{4} [V_T + V_B] \quad V_C = \frac{1}{4} [V_T + V_B]$$

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Rectangular Coaxial Cable

Original problem Computational domain



Assuming $\Delta x = \Delta y = 1$, $a = 2.5, b = 1.5, w = 1.5, d = .25$. All dimensions are in mm.

$$V_c = \frac{1}{[\epsilon_1 + \epsilon_2 + \epsilon_3 + \epsilon_4]} \left[V_T \left(\frac{\epsilon_1 + \epsilon_2}{2} \right) + V_L \left(\frac{\epsilon_1 + \epsilon_4}{2} \right) + V_B \left(\frac{\epsilon_2 + \epsilon_3}{2} \right) + V_R \left(\frac{\epsilon_3 + \epsilon_4}{2} \right) \right]$$

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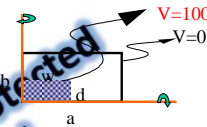
MatLab Program for the Rectangular Coaxial Cable

```

% Rect_coaxial Potential.m Started on September 5, 2011
% by: Dr. Atef Z. Elsherbeni, atef@olemiss.edu
% Potential Distribution = rectangular coaxial
% Basic solution
% Symmetry along x and y is used, hence, only one quarter only
a = 2.5; % outer length along x
b = 1.5; % outer length along y
w = 0.5; % center conductor length along x
d = 0.25; % center conductor length along y
vcond = 100; % potential of inner conductor
h = .05; % thickness of conductor
% << enter integer values >>

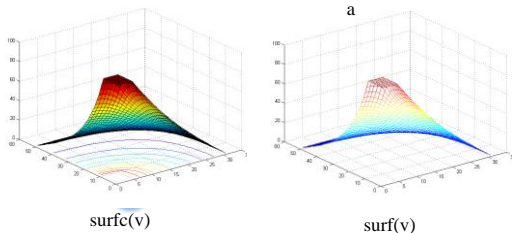
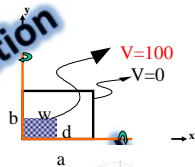
niter = 300; % iterations
nx = a/h; ny = b/h; % nx = w/h; nd = d/h
v(1:nx,1:ny) = 0; % Initialization of all nodes to zero
for i = 1:nx
    for j = 1:ny
        if i <= nx & j <= ny
            v(i,j) = vcond; % fixed potential
        elseif i == 1 & j > nd
            v(i,j) = .25*(2.*v(i+1,j)+v(i+2,j)); % symmetry along y
        elseif j == 1 & i > dw
            v(i,j) = .25*(2.*v(i+1,j)+v(i+2,j)); % symmetry along x
        else
            v(i,j) = .25*(v(i+1,j)+v(i-1,j)+v(i,j+1)+v(i,j-1)); % general point
        end
    end
end
end

surf(v); % plot the potential distribution Note the transpose operation
axis([1 nx 1 ny]); xlabel('x Axis'); ylabel('y Axis');
title('Potential Distribution'); view([-15,35]);
    
```



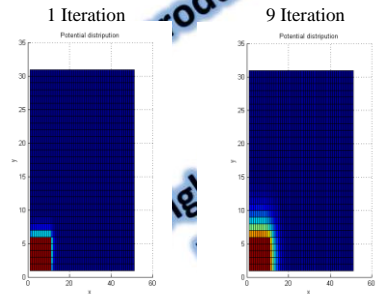
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Potential Distribution of a Rectangular Coaxial Cable



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Progress of the Iterative Solution

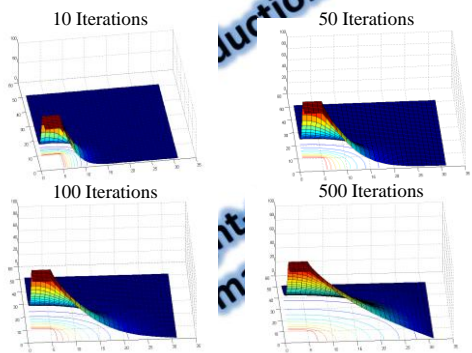


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Potential Distribution Based on the Number of Iterations



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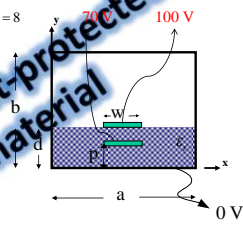
20

Home Work # 3: Potential Calculation

Develop a program to solve for the potential at all points in the shown computational domain. Use the symmetry where possible.

Keep track of the CPU time for each section of the code and for the entire code.

$a = 8, b = 6, \epsilon = 2.5, p = 1, w = 1.5, \epsilon_r = 8$
 Thickness of any of the two strips is 0.1
 All dimensions are in mm

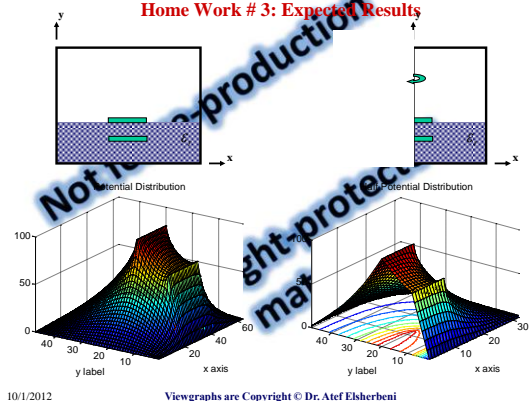


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Home Work # 3: Expected Results

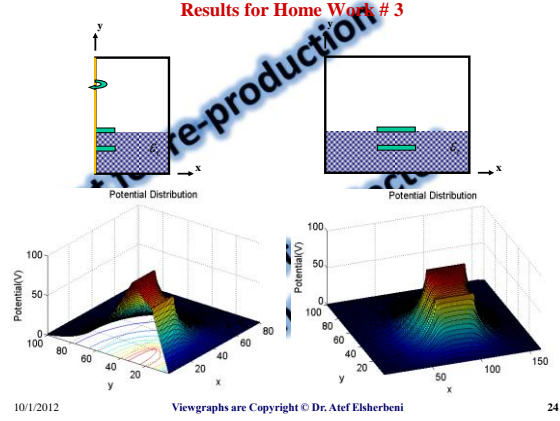


End of Lectures

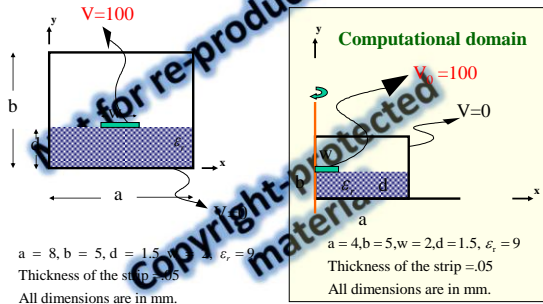
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Results for Home Work # 3



Computational Domain for The Microstrip Line Problem



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MatLab Program for The Microstrip Line Problem – 1/3

```

% Micro_Strip_Line.m Started Sep/20/1999
% by: Dr. Atef Elsherbeni, atef@olemiss.edu
% Computation of the potential distribution for a shielded microstrip line
% Symmetry along y is used
% Last modified August 2008

clear all, clf
eps0 = 8.854187817e-12; % free space permittivity
c = 2.99792458e8; % speed of light

% Input parameters
a = 8; % half of the outer length along x
b = 5; % half of the outer length along y
w = 2/2; % half of the center conductor width along x
epsr = 9.0; % relative permittivity of the dielectric substrate
eps1 = 1; % top (region 1) air dielectric
eps2 = epsr; % Bottom (region 2) dielectric
d = 1.5; % lower Y coordinate of the center conductor
% and the top coordinate of the dielectric substrate
t = .05; % thickness of the strip
% use the value of x as a scalar or multiple integer of t
vcond = 100; % potential of the center conductor
h = .05; % since h of segmentation
Maxiter = 1000; % Maximum number of iterations
% End of Input Parameters
    
```

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MatLab Program for The Microstrip Line Problem – 2/3

```

eps12 = eps1+eps2;
nx = round(a/h); ny = round(b/h);
nw = round(w/h); nd = round(d/h);
v(1:nx+1,1:ny+1) = 0.0; % initialize all nodes to zero
v(1:nw,nd:nd+nt-1) = vcond; % initialize the constant voltage

for k = 1:Maxiter
    for i = 1:nx
        for j = 1:ny
            v(i,j) = .5*(v(i+1,j)+v(i,j+1)); % average along x and y (origin point)
            elseif i <= nw & nd <= j & j <= nd+nt-1
                v(i,j) = vcond; % average along x and y (center conductor)
            elseif i == 1 & (j <= nd | j >= nd+nt-1)
                v(i,j) = -.25*(2.*v(i+1,j)+v(i,j+1)+v(i,j-1)); % symmetry along y
            elseif i > nw & j == nd+nt-1
                v(i,j) = (1/(2*(eps1+eps2))) * ((eps1-eps2)/2) * v(i+1,j) + v(i,j+1)...
                    + eps2 * (v(i+1,j) + v(i-1,j)); % potential across 2 media
            else
                v(i,j) = (.25*(v(i+1,j)+v(i-1,j)+v(i,j+1)+v(i,j-1))); % general point
            end
        end
    end
end
    
```

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