

Q10 Roadway :-

→ HZ stiffener :-

b_{st} = (60 - 1.8) / 2 = 29.1 cm → b_{st} = 25 cm

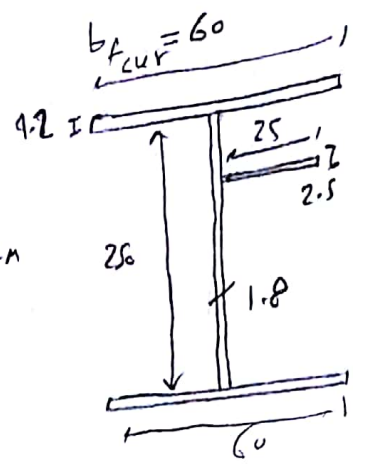
B_{st} / t_{st} ≤ 21 / √3.6 → t_{st} ≥ 2.25 cm → t_{st} = 2.5 cm

I_{st} = (25³ × 2.5) / 3 = 13020.83 cm⁴

Check Moment :-

I_{mm} = A × 250 × 1.8² = 5832 cm⁴ < I_{st}

- Use stiffeners (25 × 2.5) cm at d/5 from comp. flange



→ VL Stiffener :-

B_{st min} = (250 / 30) + 5 = 13.3 cm → B_{st} = 15 cm [2 sides]

B_{st} / t_{st} ≤ 21 / √3.6 → t_{st} ≥ 1.31 → t_{st} = 1.6 cm
Q_{all} = 236.8 t, Q_b = 0.703 t/cm²

C_s = 0.65 [(0.35 × 3.6) / 0.703 - 1] × 236.8 = 121.96 t

A = 2 × 15 × 1.6 + 25 × 1.8² = 129 cm²

I = (2 × 15 + 1.8)³ × 1.6 / 12 = 4287.66 cm⁴

C = √(I / A) = 5.77 cm, l = 0.8 × 250 = 200 cm

λ = 200 / 5.77 = 34.66

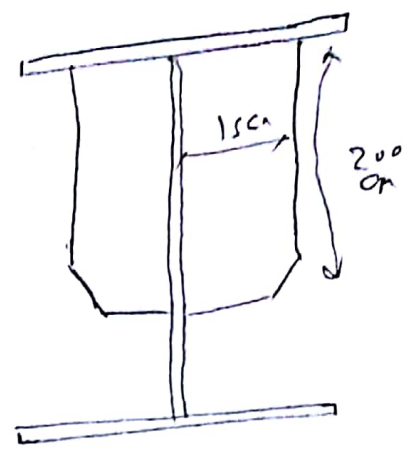
f_{cr} = 2.1 - 0.000135 × λ² = 1.938 t/cm²

$$f_{c_{act}} = \frac{121.96}{129} = 0.95 \text{ t/cm}^2 < f_{c_{all}} \quad \text{o.k.}$$

Design of well :-

$$s_w = \frac{121.96}{2 \times 2 \times \frac{250}{3} + 0.2 \times 5.1} = 0.35 \text{ cm}$$

let $s_w = 16 \text{ mm}$
min



Bearing stiffener :-

use $b_{st} = 25 \text{ cm}$

- < $\frac{60 - 1.8}{2} = 29.1 \text{ cm}$
- > $\frac{250}{10} + 5 = 15.5 \text{ cm}$
- > $\frac{60}{4} = 15 \text{ cm}$

$$\frac{b_s}{t_s} \leq \frac{21}{\sqrt{f_s}} \rightarrow \frac{25}{2\sqrt{f_s}} \leq t_s \rightarrow t_s = 2.26 \text{ cm}$$

let $t_s = 2.4 \text{ cm}$

$$\text{Area} = 2 \times 25 \times 2.4 + 12 \times 1.8^2 = 158.88 \text{ cm}^2$$

$$I = \frac{(2 \times 25 + 1.8)^3 \times 2.4}{12} = 27798.37 \text{ cm}^4$$

$$C = \sqrt{\frac{I}{A}} = 13.23 \text{ cm}$$

$$L = 0.8 \times 250 = 200 \text{ cm}$$

$$k = \frac{200}{13.23} = 15.11$$

$$P_{c_{all}} = 2.1 - 0.000135 \times k^2 = 2.07 \text{ t/cm}^2$$

$$f_{c_{act}} = \frac{236.85}{158.88} = 1.49 \text{ t/cm}^2 < f_{c_{all}} \quad \text{o.k.}$$

→ Check bearing

$$f_{bearing} = \frac{236.8}{(25-2) \times 2.4 \times 2} = 2.15 \text{ t/cm}^2 < 2 \times 2.1 \text{ t/cm}^2$$

0.15

→ weld design

$$S_w = \frac{236.8}{(250-4) \times 4 \times 0.2 \times 5.2} = 0.23 \text{ cm}$$

$$S_w = 6 \text{ mm}$$

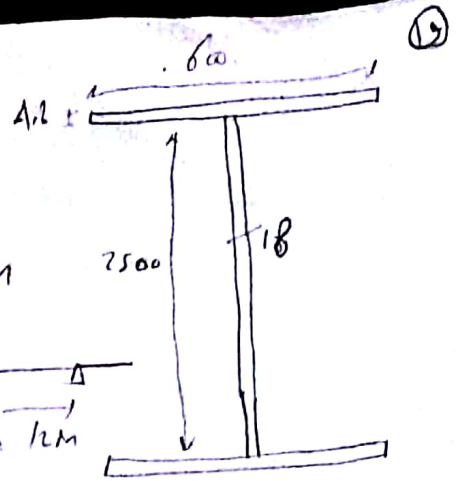
min

Q11

$$Z_x = 31163.42 \text{ cm}^3$$

$$I_{cur} = 10486313.52 \text{ cm}^4$$

location of splice:- at curtailment location



$$\therefore M_{capacity} = 31163.42 \times 21$$

$$= 170443.182 \text{ t.cm}$$

$$Q_{splice} = Q_{cur} = 101.48 \text{ t}$$

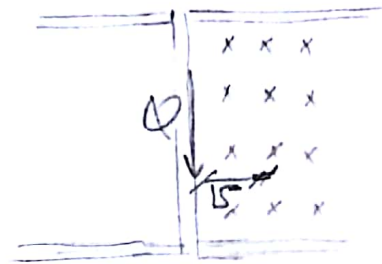
→ Web splice

assume spacing between bolts = 10cm

$$\text{No. bolts / col} = \frac{250 - 10}{10} = 24 \text{ bolts}$$

$$e = 5 \text{ cm}$$

- assume using 3 columns of bolts



- S.A on splice

$$Q_y = 101.48 \text{ t}$$

$$M_w = 170443.182 \times \frac{1.8 \times 250^3}{12} = 38095.01 \text{ t.cm}$$

$$M_z = 38095.01 + 101.48 \times 15 = 39617.21 \text{ t.cm}$$

$$Q_{y/b} = \frac{101.48}{3 \times 24} = 1.41 \text{ t}$$

$$\sum Y^2 = 2 \times 10^2 \times 24 + 2 \times (5^2 + 15^2 + 25^2 + 35^2 + 45^2 + 55^2 + 65^2 + 75^2 + 85^2 + 95^2 + 105^2 + 115^2) \times 3$$

$$= 349800 \text{ cm}^2$$

$$Q_{y/bolt} = \frac{39617.21}{349800} \times 16 = 1.13 \text{ t}$$

$$Q_{x/bolt} = \frac{39617.21}{349800} \times 15 = 13.02$$

$$Q_{bolt} = \sqrt{(1.13 + 1.13)^2 + 13.02^2} = 13.26 \text{ t}$$

13.26 = 2 * P_s ~> P_s = 6.63 t

Use 24 M 24 (10.5) -> P_s = 6.94 t

Design of plate:-

A_w = 250 * 1.8 = 450 cm^2

450 = 2 * 240 * t_p ~> t_p = 0.94 cm

t_p = 1 cm

I_w = (1.8 * 250^3) / 12 = I_p = (2 * t_p * 240^3) / 12

t_p2 = 1.08 cm

t_p = 1.2 cm

Use 2 PL 2400 * 12 mm

Plate splice:-

assume using 4 bolts / row

M_plate = 170443.182 - 38095.01 = 132348.172 t.cm

T_c = (132348.172) / (250 + 48) = 520.65 t

assume using M 24

n = (520.65) / (2 * 6.79) = 37.9 ~ 40 bolts

No. of rows = (40) / 4 = 10 row

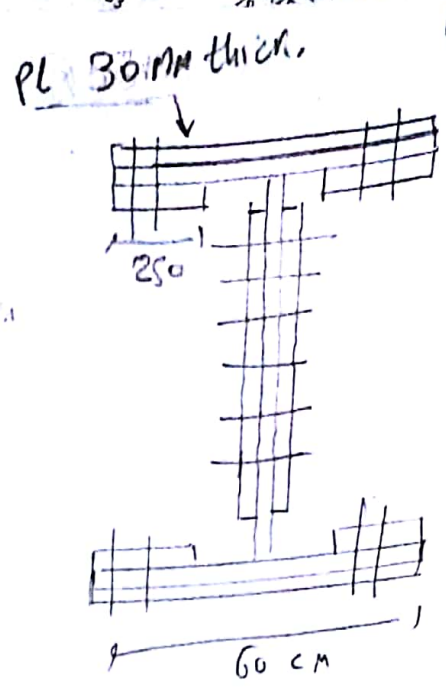
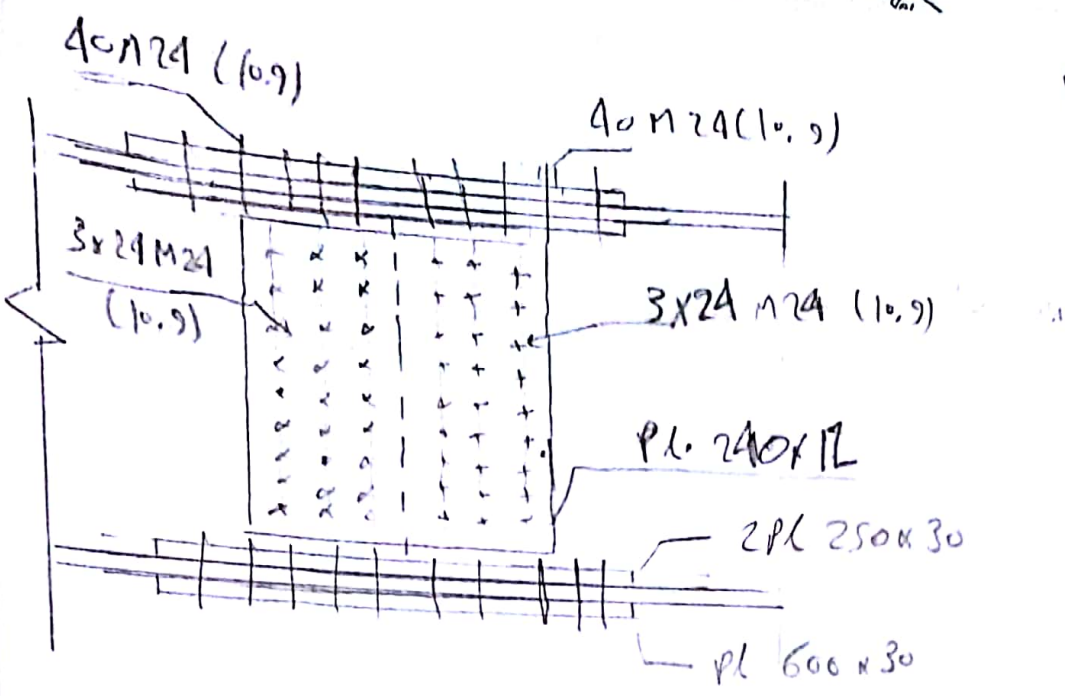
Bearing t_w = (60 - 1.8) / 2 = 29.1 cm > 6 * 2.9 cm

Design of plate:-

A_p = (520.65) / 2.1 = 247.93 cm^2 (assume) b_1 = 60 cm, b_2 = 25 cm / 60

247.93 = (60 + 2 * 2.5 * (8 * 2.1)) * t_p

t_p = 2.73 cm ~ 3 cm



(21)

